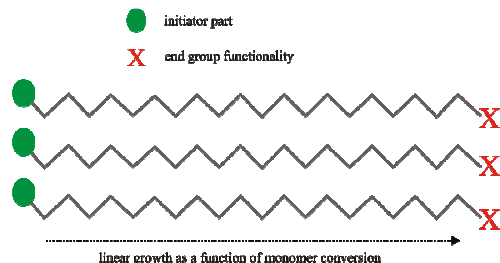
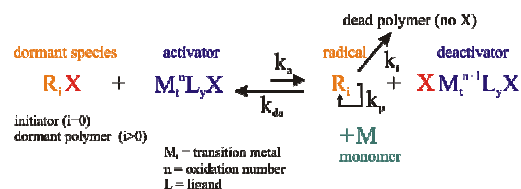


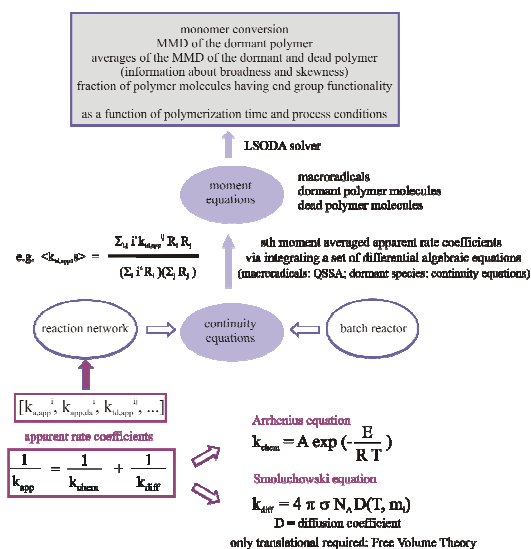
## Objectives of ATRP



## Reaction mechanism of ATRP

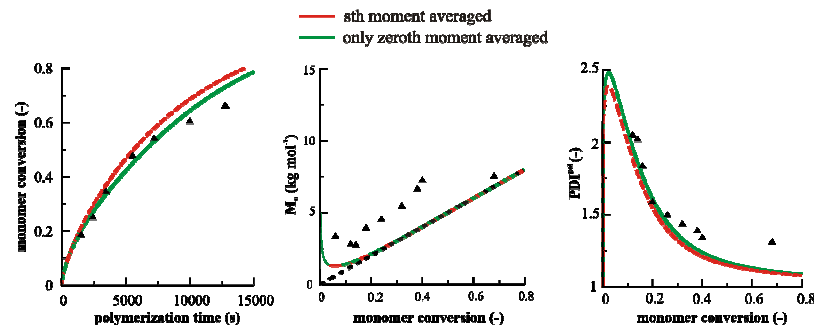


## Modeling strategy



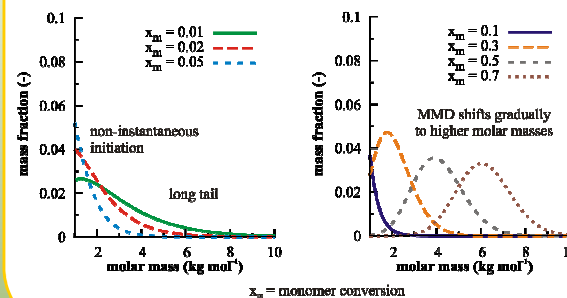
D'hooge et al., *Macromol. Rapid. Commun.*, 2004, 25(1), 1-10; *Macromol. Rapid. Commun.*, 2008, 29(1), 1-10

## Comparison with experimental data

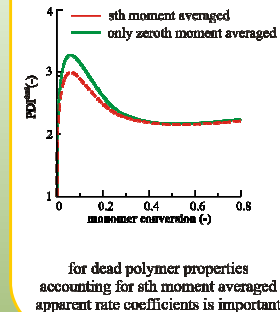


[MMA]<sub>0</sub> / [R<sub>2</sub>X]<sub>0</sub> / [Cu(I)Br]<sub>0</sub> / [PMDETA]<sub>0</sub> = 100/1/0.5/0.5; [MMA]<sub>0</sub> = 3100 mol m<sup>-3</sup>; [Cu(I)Br]<sub>0</sub> = 0 mol m<sup>-3</sup>  
polymerization temperature: 363 K; solvent: toluene; MMA: methyl methacrylate; R<sub>2</sub>X: ethyl 2-bromo isobutyrate  
PMDETA: N,N,N',N'',N''-pentamethyldiethylene-triamine  
Experimental data: Snijder et al., *Macromolecules* 2002, 35, 4785

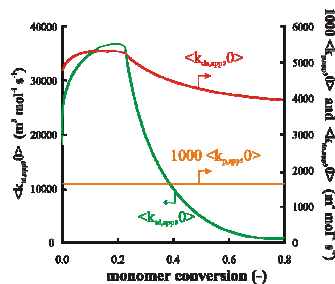
## MMD of the dormant polymer



## Dead polymer



## Diffusional limitations



## Conclusions

The monomer conversion, the MMD of the dormant polymer, averages of the MMD of the dead and dormant polymer are calculated as a function of polymerization time and process conditions, while accounting for diffusional limitations on all reaction steps in a fundamental way. Simulation results are in agreement with experimental data from literature.

## Acknowledgments

The Institute for the promotion of Innovation through Science and Technology in Flanders (IWT Vlaanderen) and the Belgian Government (IAP/IUAP/PAI P6/27: "Functional Supramolecular Systems") are acknowledged for financial support.